



## **BDA016 Stavební mechanika 2**

### **6. přednáška**

- Rovinný rám řešený silovou metodou

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V přednášce jsou použity obrázky z učebnice Kadlčák, J., Kytýr, J. Statika stavebních konstrukcí II. Staticky neurčité prutové konstrukce. Nakladatelství VUTIUM v Brně, 2004.

## Stupeň statické neurčitosti

- $n_s = r - m = 6 - 3 = 3$

## Základní soustava – SU

- odebrání 3 vazeb

## Staticky neurčité veličiny

- 3 složky reakcí

- $X_1 = M_a$

- $X_2 = M_b$

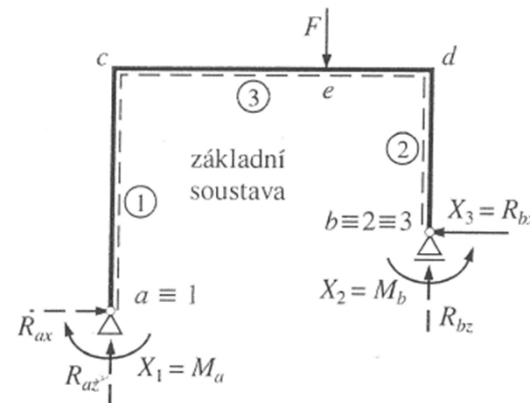
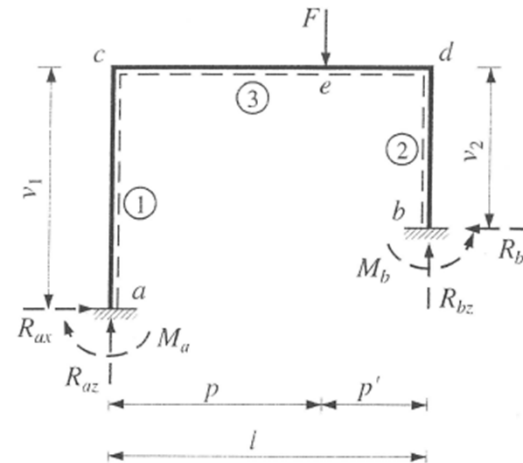
- $X_3 = R_{bx}$

## Deformační podmínky

- $\delta_1 = \varphi_a = 0$

- $\delta_2 = \varphi_b = 0$

- $\delta_3 = u_b = 0$



## Princip superpozice → 4 zatěžovací stavy

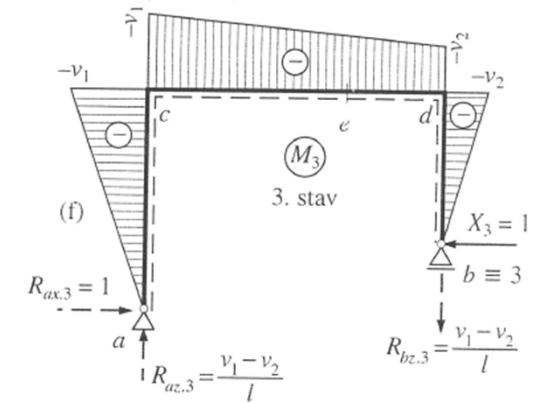
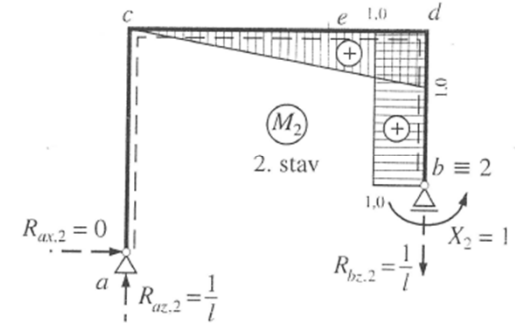
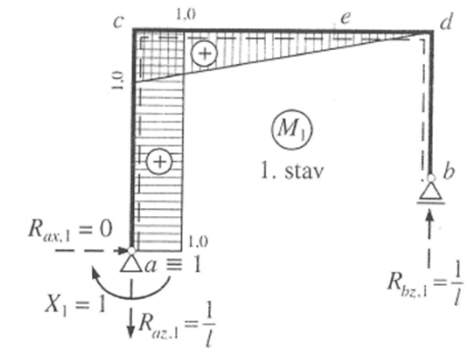
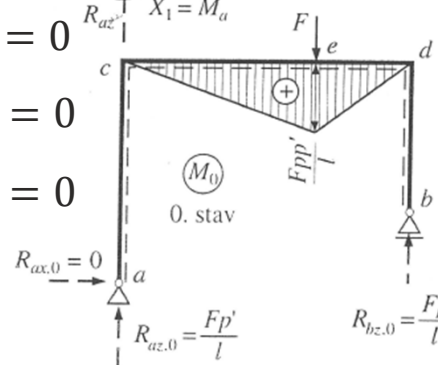
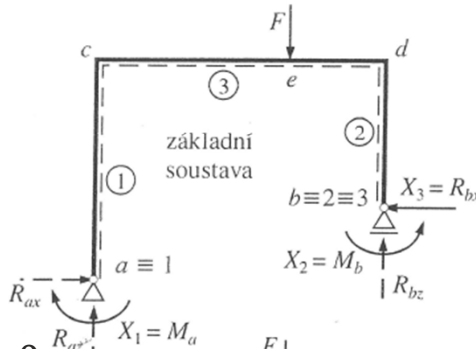
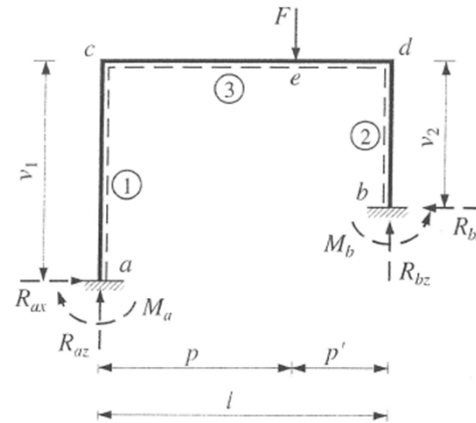
- 0. ZS – zatížení
- 1. ZS –  $X_1 = M_a = 1$
- 2. ZS –  $X_2 = M_b = 1$
- 3. ZS –  $X_3 = R_{bx} = 1$

## Systém lineárních rovnic

- $\delta_1 = \delta_{10} + \delta_{11} \cdot X_1 + \delta_{12} \cdot X_2 + \delta_{13} \cdot X_3 = 0$
- $\delta_2 = \delta_{20} + \delta_{21} \cdot X_1 + \delta_{22} \cdot X_2 + \delta_{23} \cdot X_3 = 0$
- $\delta_3 = \delta_{30} + \delta_{31} \cdot X_1 + \delta_{32} \cdot X_2 + \delta_{33} \cdot X_3 = 0$

## kanonické rovnice silové metody

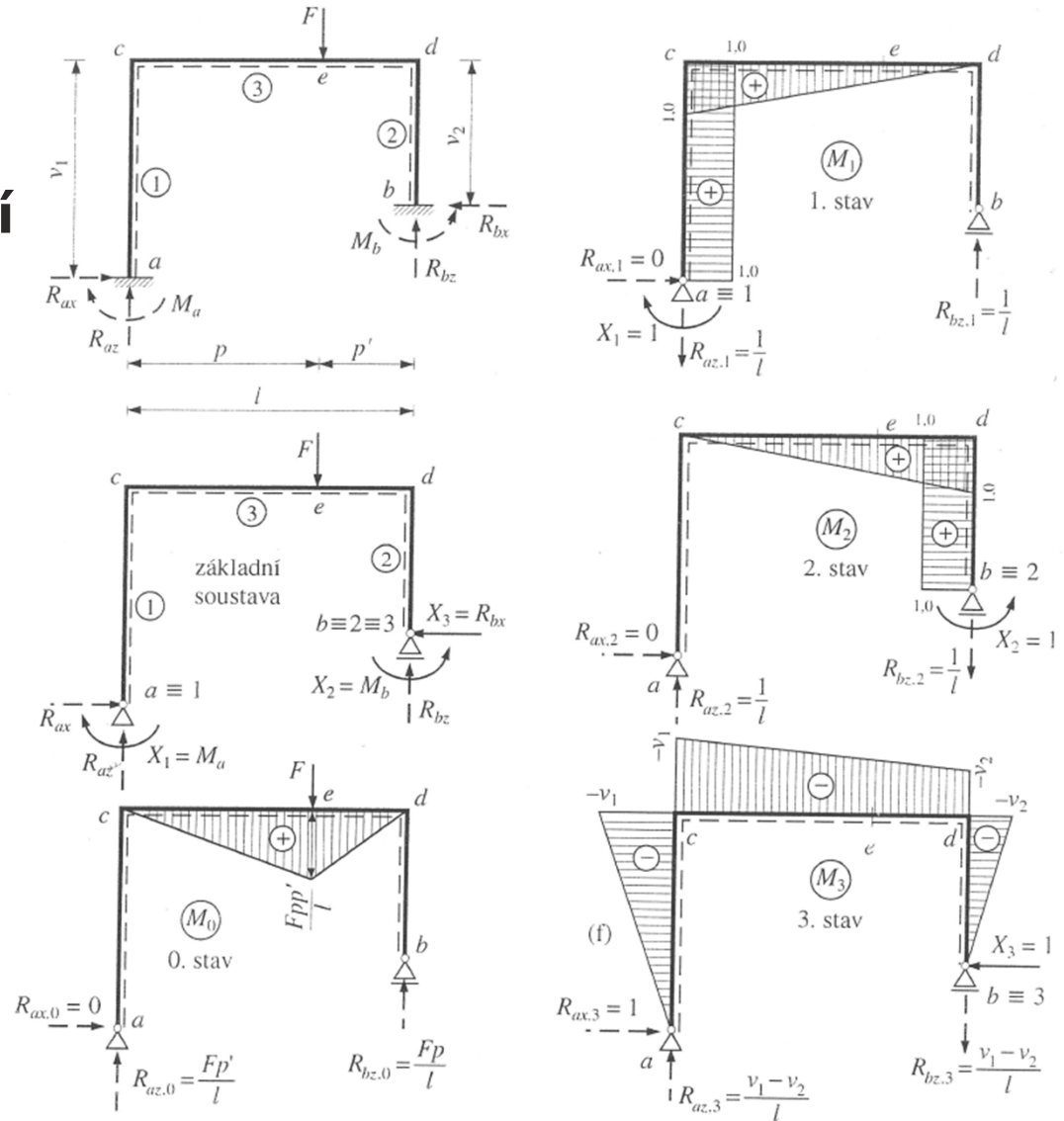
- $\sum_{k=1}^{n_s} \delta_{ik} \cdot X_k + \delta_{i0} = 0$



## Deformační součinitele

→ z principu virtuálních prací  
pro silové zatížení

- $\delta_{i0} = \int_0^s \frac{N_i N_0}{EA} ds + \int_0^s \kappa \frac{V_i V_0}{GA} ds + \int_0^s \frac{M_i M_0}{EI} ds$
- $\delta_{ik} = \int_0^s \frac{N_i N_k}{EA} ds + \int_0^s \kappa \frac{V_i V_k}{GA} ds + \int_0^s \frac{M_i M_k}{EI} ds$
- $i = 1, 2, \dots, n_s$
- $\delta_{ik} = \delta_{ki}$



## Stupeň statické neurčitosti

- $n_s = r - m = 6 - 3 = 3$
- $n_s = 3 \cdot 1 - 0 + (3 - 3) = 3$

## Základní soustava – SU

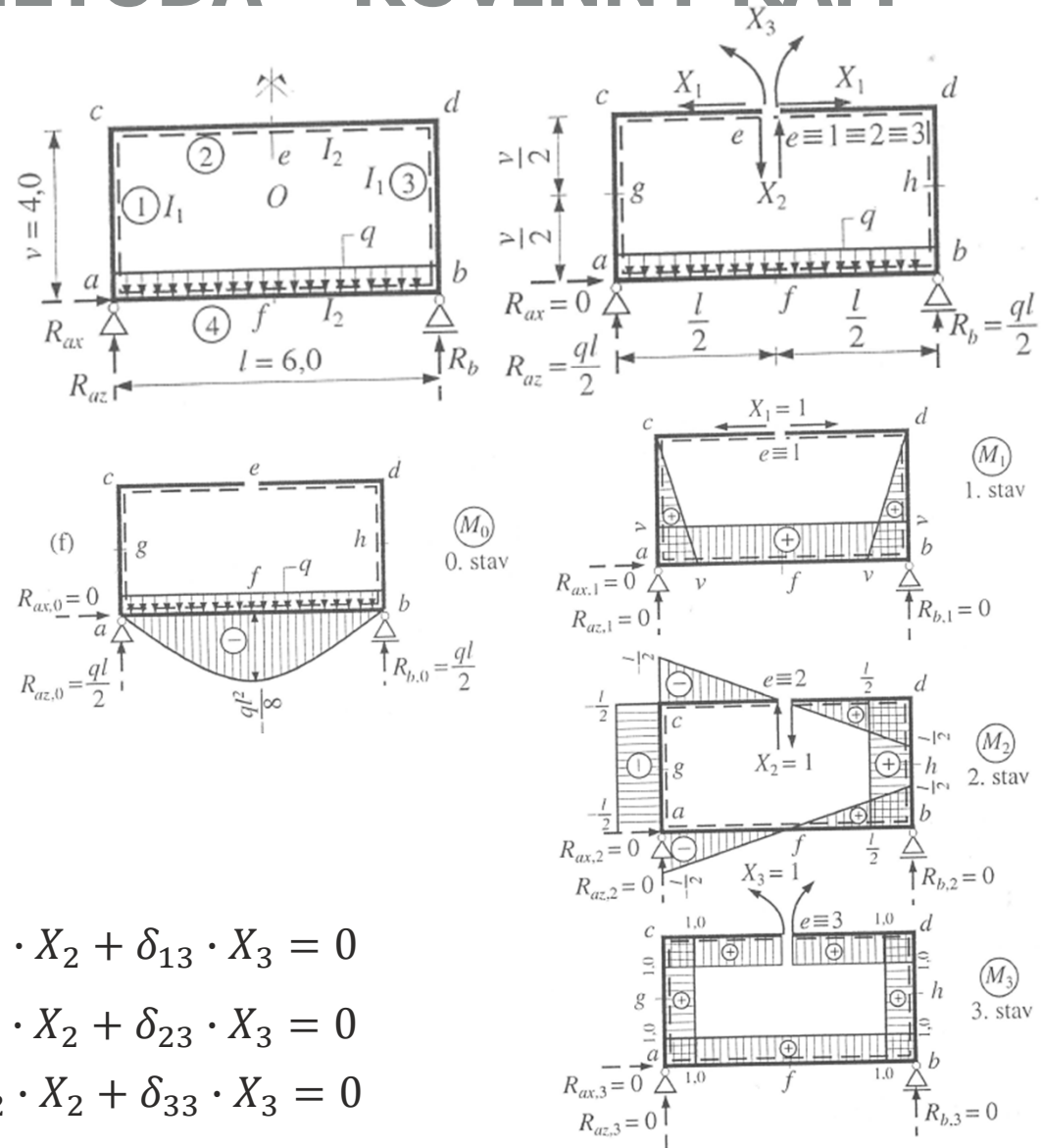
- odebrání 3 vazeb – vnitřní

## Staticky neurčité veličiny

- 3 složky výslednice vnitřních sil
- $X_1 = N_e$
- $X_2 = V_e$
- $X_3 = M_e$

## Deformační podmínky

- $\delta_1 = u_{ee} = 0: \delta_{10} + \delta_{11} \cdot X_1 + \delta_{12} \cdot X_2 + \delta_{13} \cdot X_3 = 0$
- $\delta_2 = w_{ee} = 0: \delta_{20} + \delta_{21} \cdot X_1 + \delta_{22} \cdot X_2 + \delta_{23} \cdot X_3 = 0$
- $\delta_3 = \varphi_{ee} = 0: \delta_{30} + \delta_{31} \cdot X_1 + \delta_{32} \cdot X_2 + \delta_{33} \cdot X_3 = 0$



## Deformační součinitele

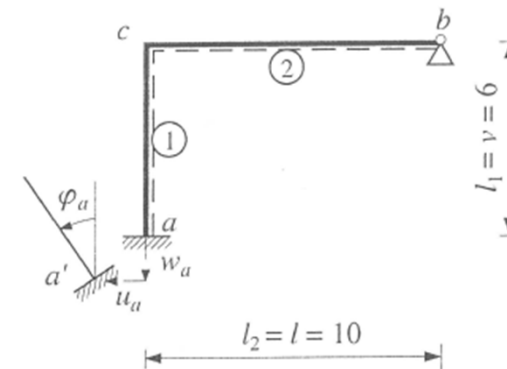
→ z principu virtuálních prací  
pro teplotní zatížení

$$\delta_{i0,t} = \int_0^S N_i \alpha_t \Delta T_0 ds + \int_0^S M_i \alpha_t \frac{\Delta T}{h} ds$$

## pro popuštění podpor

- popuštění je zadané v místě odebrané vazby  
→ popuštění se objeví na pravé straně rovnice
- popuštění je zadané v místě ponechané vazby  
→ popuštění se uvažuje v 0.ZS

$$\begin{aligned} \delta_{i0,p} &= - \sum_{r=1}^{p_v} R_{r,i} \cdot \delta_r = \\ &= - \sum_{r=1}^{p_v} (R_{rx,i} \cdot u_r + R_{rz,i} \cdot w_r + R_{rM,i} \cdot \varphi_r) \end{aligned}$$



Na dané konstrukci pomocí silové metody vykreslete průběhy vnitřních sil.

$$E = 210 \text{ GPa}$$

$$I = 2 \cdot 10^{-5} \text{ m}^4$$

$$h = 0,2 \text{ m}$$

$$\alpha_t = 1,2 \cdot 10^{-5} \text{ }^\circ\text{C}^{-1}$$

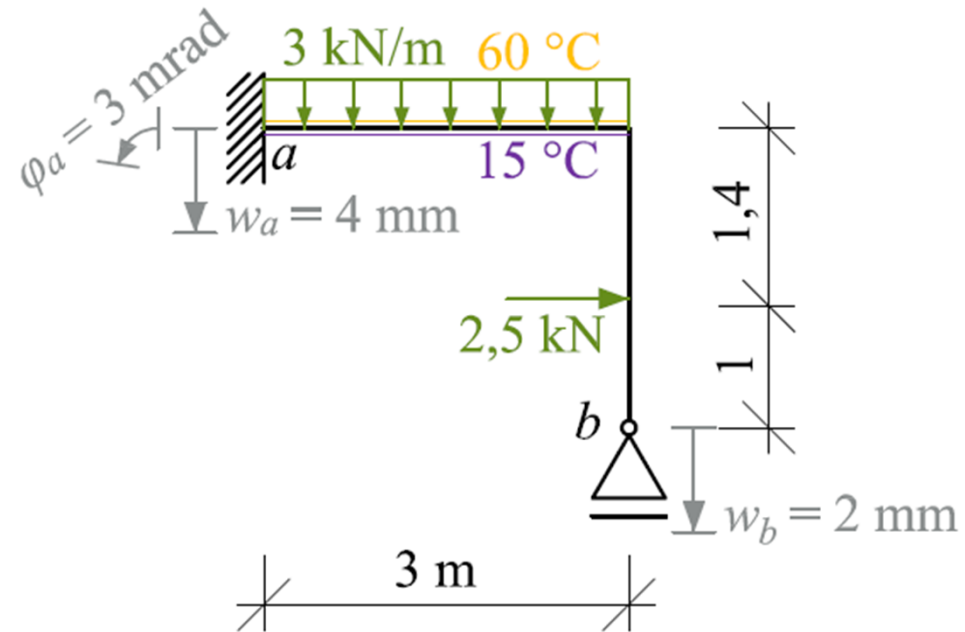
$$EI = 4,2 \cdot 10^6 \text{ Nm}^2$$

$$\Delta T_d = 15 \text{ }^\circ\text{C}$$

$$\Delta T_h = 60 \text{ }^\circ\text{C}$$

$$\Delta T_0 = \frac{\Delta T_d + \Delta T_h}{2} = \frac{15 + 60}{2} = 37,5 \text{ }^\circ\text{C}$$

$$\Delta T = \Delta T_d - \Delta T_h = 15 - 60 = -45 \text{ }^\circ\text{C}$$



## Stupeň statické neurčitosti

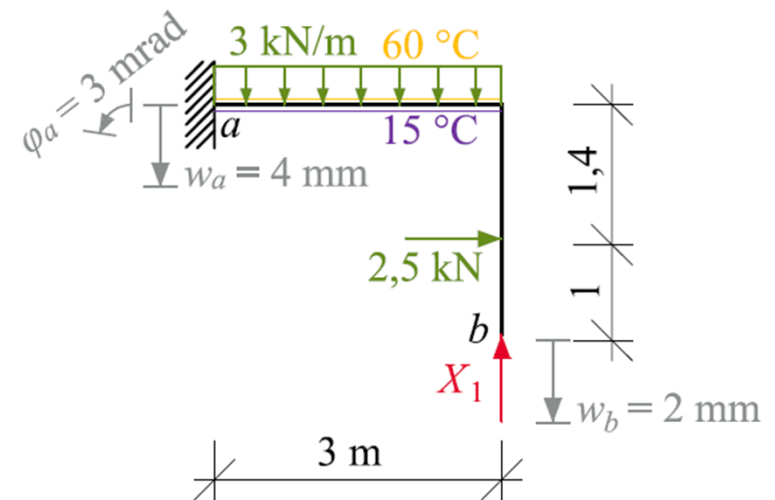
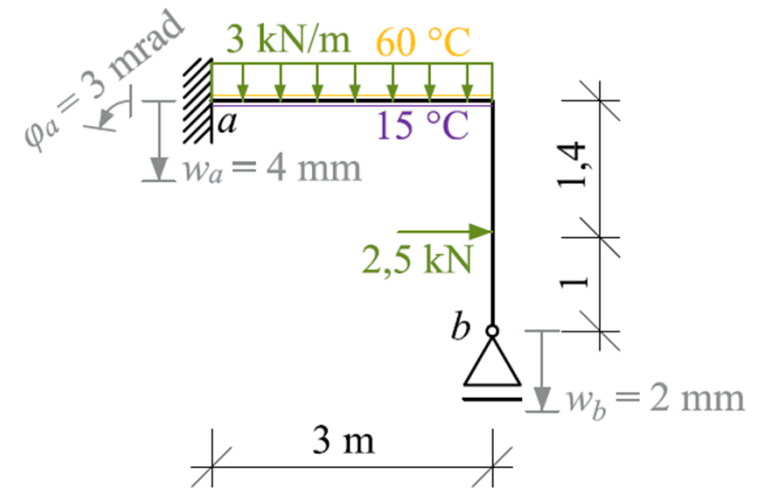
- $n_s = 4 - 3 = 1$

## Základní soustava – staticky určitá

- odebereme  $n_s$  přebytečných vazeb
- nahradíme staticky neurčitými veličinami

## Deformační podmínka

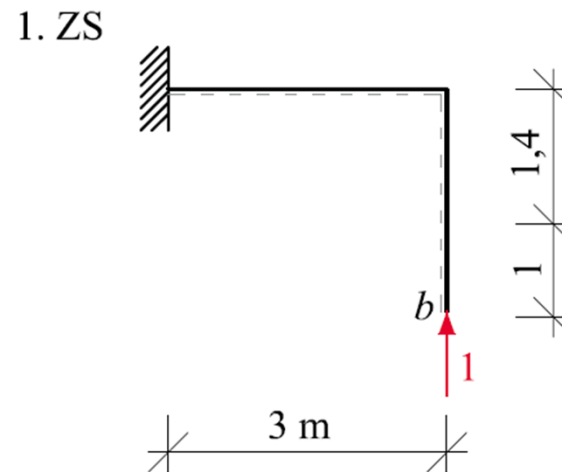
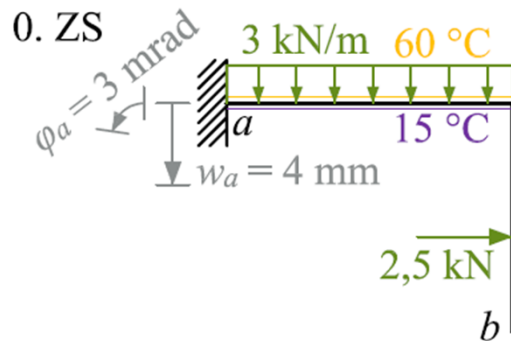
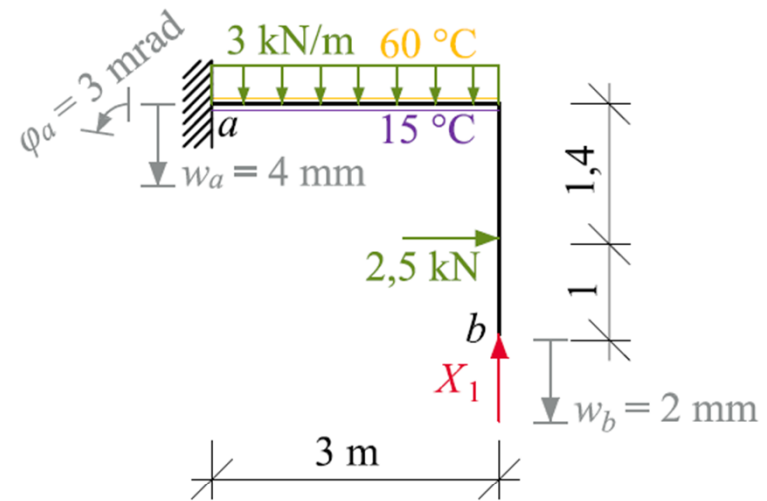
- $w_b = \delta_1 = -0,002 \text{ m}$
- $w_b = w_{b,z} + w_{b,X_1}$
- $\delta_{10} + \delta_{11} \cdot X_1 = -0,002$





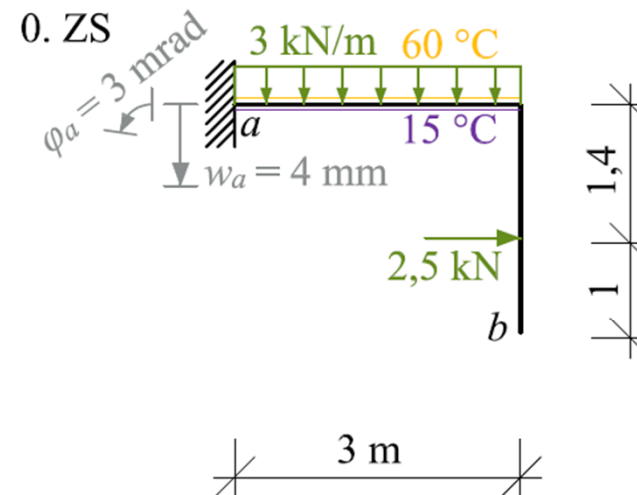
## Zatěžovací stavy – princip superpozice

- $\delta_{10} + \delta_{11} \cdot X_1 = -0,002$
- $\delta_{10} = \delta_{10,sz} + \delta_{10,t} + \delta_{10,p}$
- $\delta_{11} = \int_0^s \frac{M_1 \cdot M_1}{EI} ds$

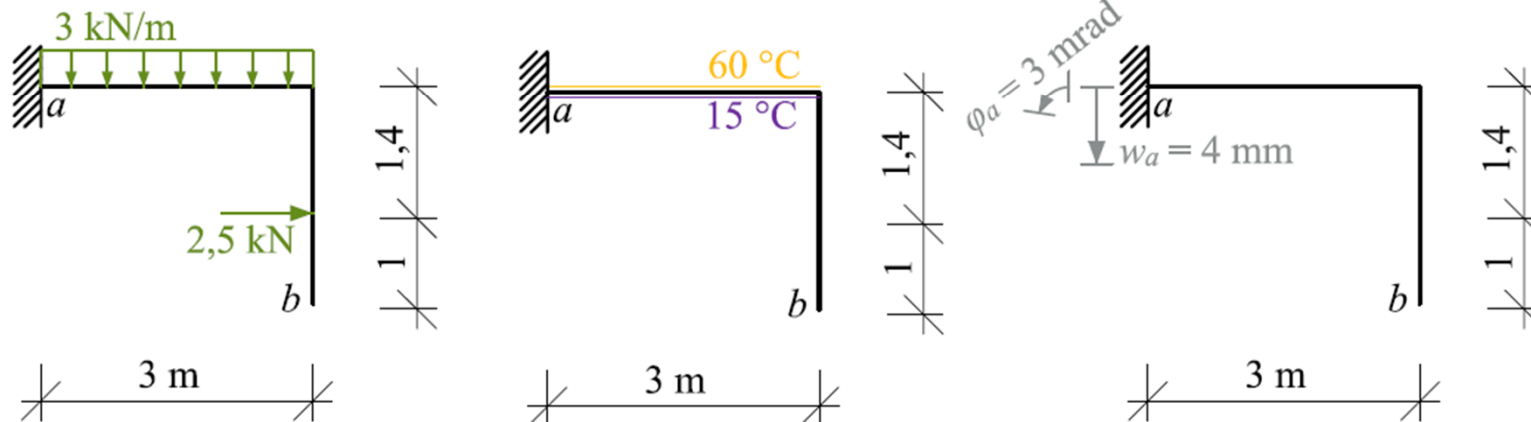


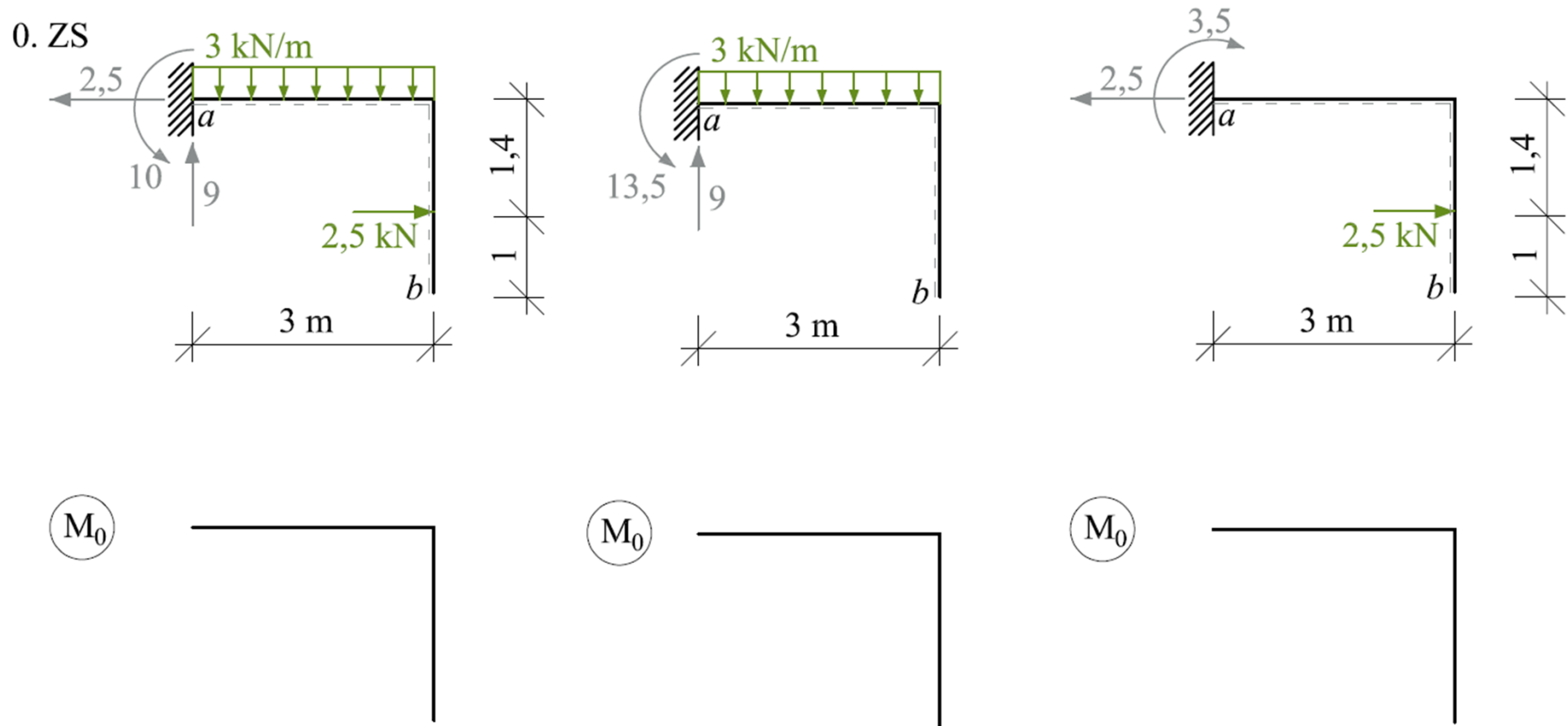
## 0.ZS

- $\delta_{10} = \delta_{10,sz} + \delta_{10,t} + \delta_{10,p}$
- $\delta_{10,sz} = \int_0^s \frac{M_1 \cdot M_0}{EI} ds$
- $\delta_{10,t} = \int_0^s N_1 \alpha_t \Delta T_0 ds + \int_0^s M_1 \alpha_t \frac{\Delta T}{h} ds$
- $\delta_{10,p} = - \sum_{r=1}^{p_v} R_{r,1} \cdot \delta_r$



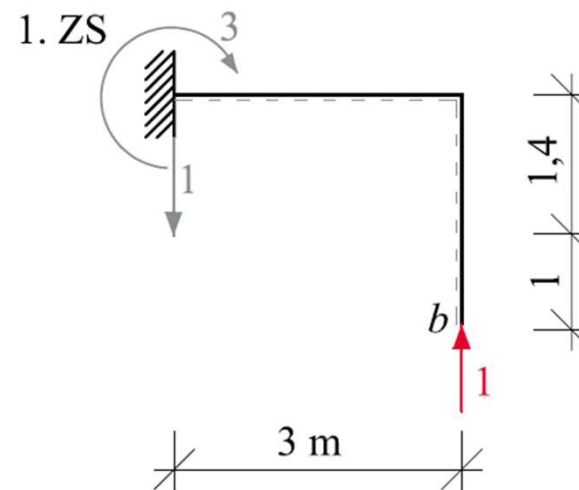
0. ZS



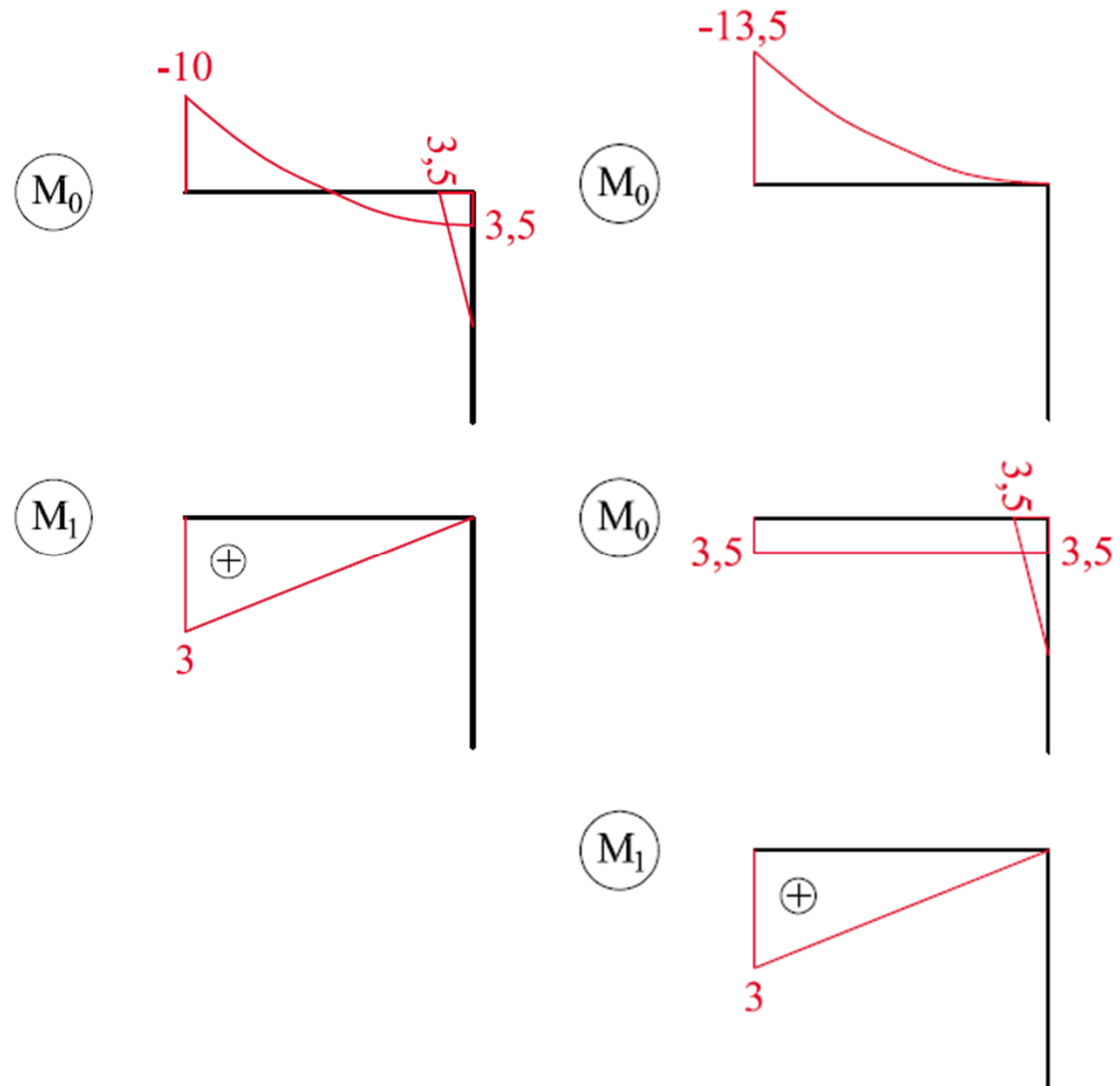


**1.ZS**

$$\delta_{11} = \int_0^s \frac{M_1 \cdot M_1}{EI} ds$$

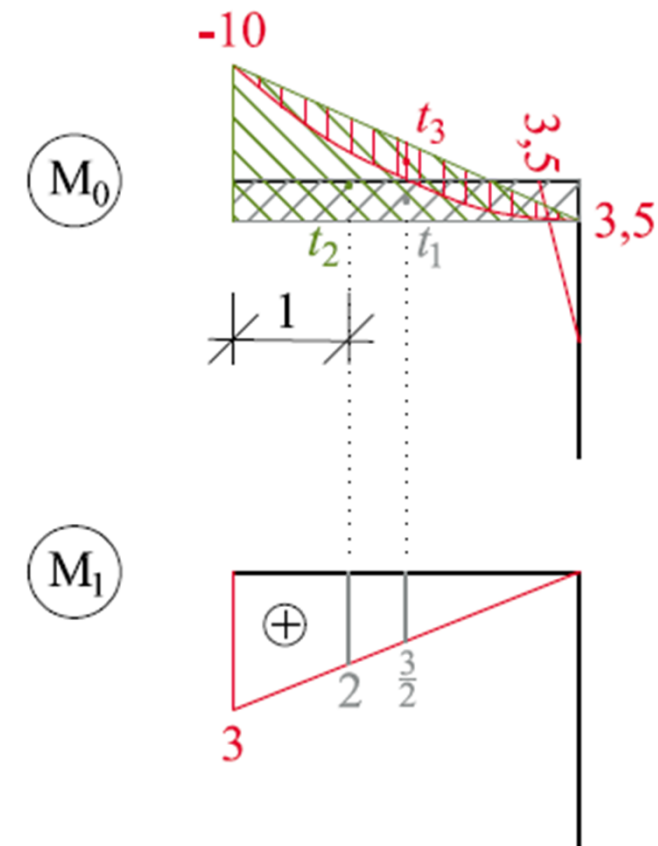


$$\delta_{10,sz} = \int_0^s \frac{M_1 \cdot M_0}{EI} ds =$$

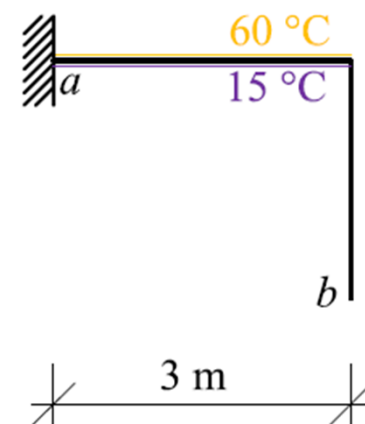


$$\begin{aligned} \delta_{10,sz} &= \int_0^s \frac{M_1 \cdot M_0}{EI} ds = \frac{1}{EI} \int_0^s M_1 \cdot M_0 ds = \\ &= \frac{1 \cdot 10^3}{4,2 \cdot 10^6} \left( 3 \cdot 3,5 \cdot \frac{3}{2} + \frac{1}{2} \cdot 3 \cdot (-13,5) \cdot 2 + \right. \\ &\quad \left. + \frac{2}{3} \cdot 3 \cdot 3,375 \cdot \frac{3}{2} \right) = \\ &= \frac{-14,625 \cdot 10^3}{4,2 \cdot 10^6} \rightarrow \end{aligned}$$

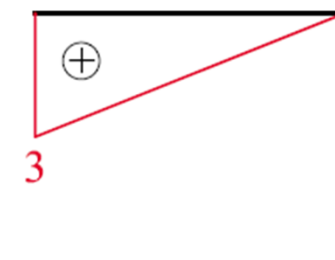
$$\delta_{10,sz} = -3,482 \cdot 10^{-3} \text{ m}$$



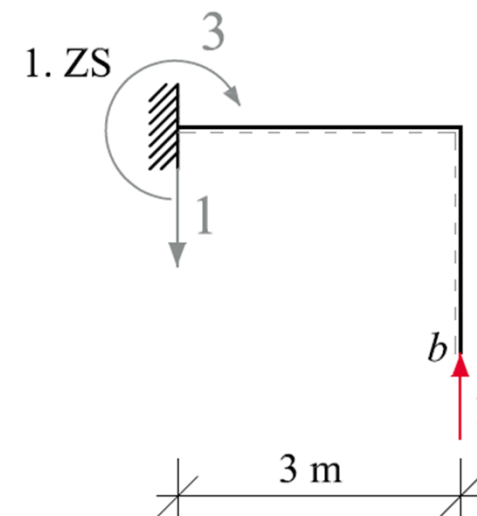
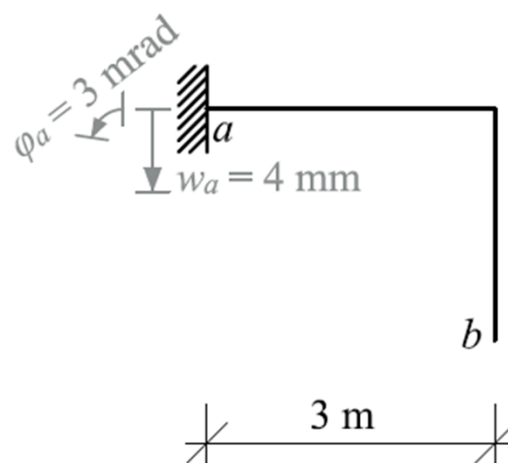
$$\delta_{10,t} = \int_0^s N_1 \alpha_t \Delta T_0 ds + \int_0^s M_1 \alpha_t \frac{\Delta T}{h} ds$$



$M_1$



$$\delta_{10,p} = - \sum_{r=1}^{p_v} R_{r,1} \cdot \delta_r$$



$$\delta_{10} + \delta_{11} \cdot X_1 = -0,002$$

$$\delta_{10} = \delta_{10,sz} + \delta_{10,t} + \delta_{10,p} =$$

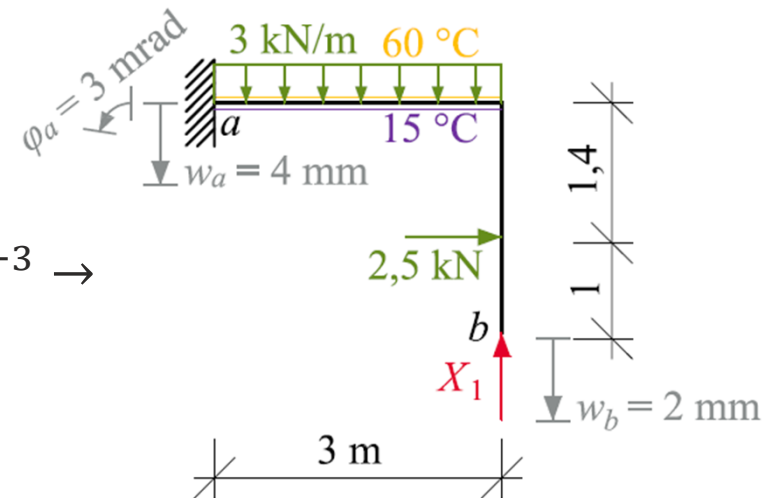
$$= -3,482 \cdot 10^{-3} + (-12,15 \cdot 10^{-3}) + 5 \cdot 10^{-3} \rightarrow$$

$$\delta_{10} = -10,632 \cdot 10^{-3} \text{ m}$$

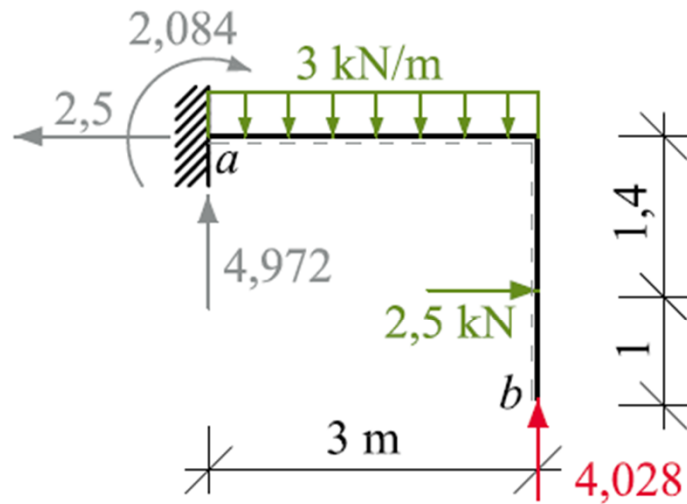
$$\delta_{11} = 2,143 \cdot 10^{-6} \frac{\text{m}}{\text{N}}$$

$$-10,632 \cdot 10^{-3} + 2,143 \cdot 10^{-6} \cdot X_1 = -0,002 \rightarrow$$

$$X_1 = 4\,028 \text{ N} = 4,028 \text{ kN}$$







(V)



(N)



(M)

